

A low-dimensional model of separation bubbles

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Introduction

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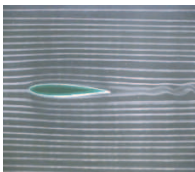
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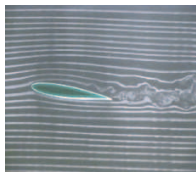
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 - model based on intuitive physical variables.

Introduction

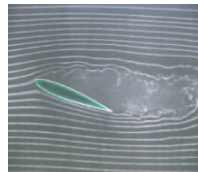
What is the separation^a?



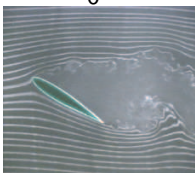
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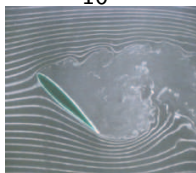
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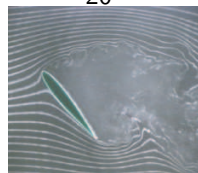
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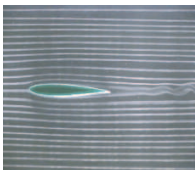


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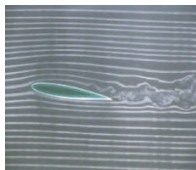
^aMultimedia Fluid Mechanics, Homsy *et al.* (2001)

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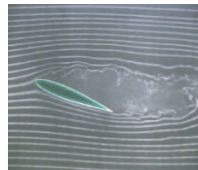
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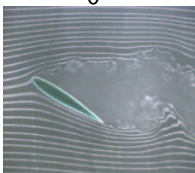
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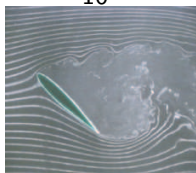
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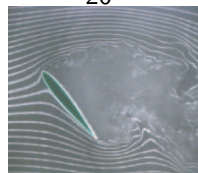
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Historical remark: term “separation bubble” is due to Jones (1933).

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- **Why control separation?:** DV shedding yields (a) losses in lift, (b) sharp increases in drag, (c) destructive pitching moments.

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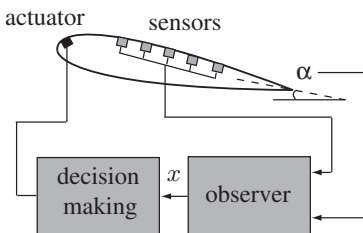
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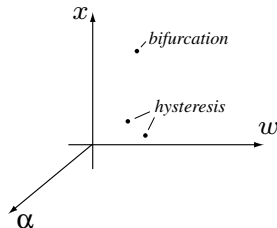
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- **How to control?:** Via *model-based observer*, which should be
 - *low-dim*, for computational efficiency in real flight;
 - *physically motivated*, to reflect actual behavior.

Introduction

Closed-loop dynamic control system



(a) Feedback control.



(b) State space.

Figure: The key dynamic elements—bifurcation and hysteresis—to be captured by the minimal number of parameters, namely the bubble size x , the angle of attack α , and the actuation amplitude w .

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Approaches to low-dimensional modeling

- **POD methods** (Kosambi, 1943)
Disadvantages: (a) unreliable for open flows, (b) physical mechanisms remain uncovered, (c) need a full solution.

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Classical example of the successful phenomenology: Landau equation (Landau, 1944; Stuart, 1960):

$$\frac{dA}{dt} = A - \gamma A |A|^2.$$

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State-of-the-art low dimensional model^a

- Physical variables:

$$\begin{array}{l} \text{(i) lift } Z \\ \text{(ii) separation state } B \end{array} = \begin{cases} 0, \text{ fully attached} \\ 1, \text{ fully separated} \end{cases}$$

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- Physical arguments:
 - (i) lift $Z \sim$ circulation $\Gamma(\alpha)$;
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 - (iii) $Z \sim B_t$ (rise in lift when a DV is shed)

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- The simplest low-order model

$$B_{tt} = -k_1 B_t + k_2 [B_s(\alpha) - B],$$

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Question: is this linear model adequate?

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Physics of actuation

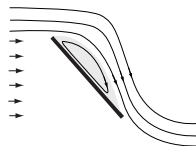
- *Mechanism*: the excitation (vs. forcing) generates Large Coherent Structures transferring high momentum fluid towards the surface:



(a) no excitation



(b) weak excitation

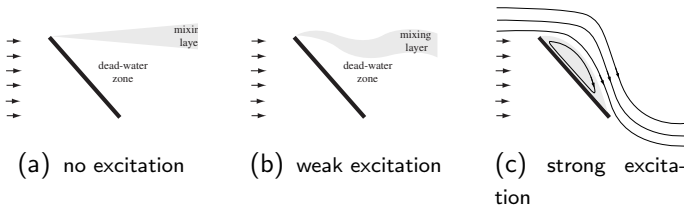


(c) strong excitation

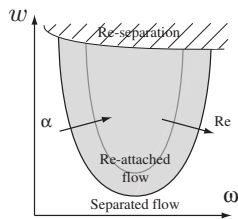
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Physics of actuation

- *Mechanism*: the excitation (vs. forcing) generates Large Coherent Structures transferring high momentum fluid towards the surface:



- *Threshold for actuation* to achieve reattachment and *effects of amplitude w and frequency ω of actuation on bubble size x* (Nishri & Wygnanski, 1998)
- *Re-separation phenomena* (Krechetnikov & Lipatov, 2000)



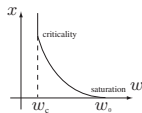
Introduction

Physics of actuation (continued)

- *Primary bifurcation* in two basic experimental models:



(a) Hump model

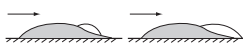


(b) Airfoil model

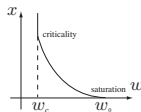
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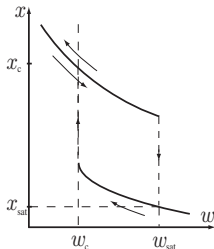


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- *Hysteresis behavior* in all (α, w, ω) , (Nishri & Wygnanski, 1998; Greenblatt *et al.* 2001).



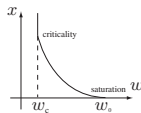
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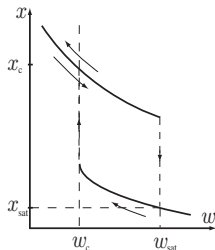
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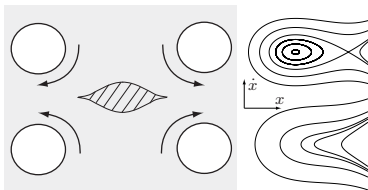
- **Conclusion:** a model should be nonlinear.



Bifurcation

Motivation from real bubbles

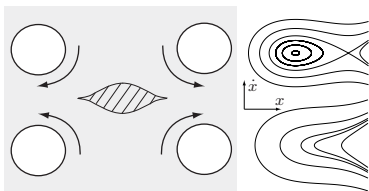
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Bifurcation

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- Let x be a scalar measure of deformation from sphericity. Linear oscillation theory (Lamb, 1932) of a spherical bubble + steady state weakly nonlinear deformation theory:

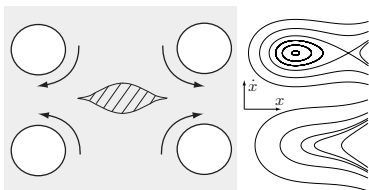
$$\ddot{x} = -\mu\dot{x} + (ax - bx^2) + w,$$

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- Bifurcation type: Takens-Bogdanov

Bifurcation

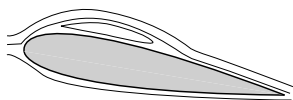
A new model: determination of variables

- Since the separation is associated with the *separation region*, it is natural to describe it with the variable representing some characteristic of a separation bubble, e.g. the *bubble size* x .

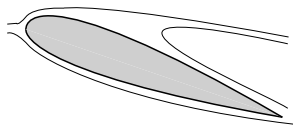
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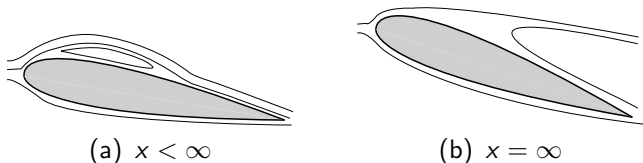


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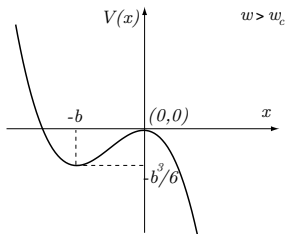
- Naturally, the bubble size $x(t; \alpha, w)$ is a function of time t , a *flight parameter*, angle of attack α , and a *control parameter* w :

$$\ddot{x} + \mu \dot{x} = F(x, w, \alpha),$$

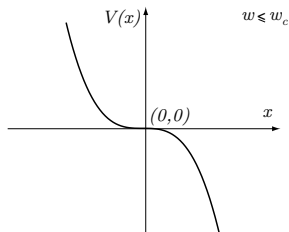
with minimal quadratic nonlinearity $F(x, w, \alpha) = x^2 + b(w, \alpha)x + c(w, \alpha)$.

Bifurcation

Potential function approach



(a) Potential function for a finite bubble.



(b) Potential function for an infinite bubble.

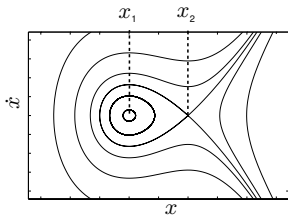
Figure: Potential function $V(x) = -\frac{x^3}{3} - b(w)\frac{x^2}{2} - c(w)x - d(w)$ with $d = 0$, $c = 0$.

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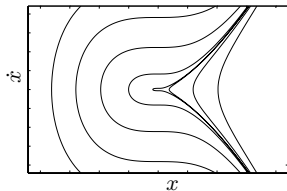
A new model: construction and analysis

- The model is a part of the Takens-Bogdanov bifurcation:

$$\ddot{x} = -\mu\dot{x} + (x - \alpha)^2 + f(w)x.$$



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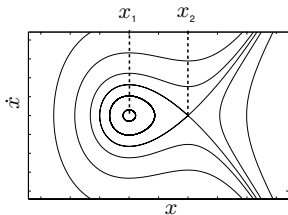
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Bifurcation

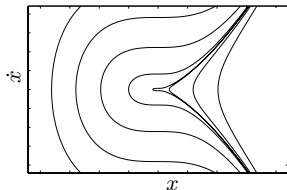
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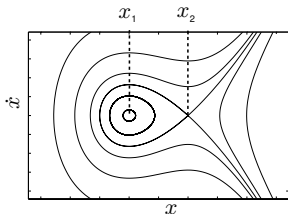
- Here $f(w) = a_1w + a_2w^2 + \dots$ represents the *nonlinear response* of the separation region to actuator excitations, for instance, of a periodic form $w = w_0 \sin \omega t$. The product $f(w)x$ means that the *effect of actuation depends upon the bubble size x* .

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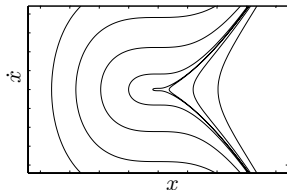
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- Prediction:** separation bubble should be finite-amplitude unstable.

Bifurcation

Concept of dynamic bifurcation

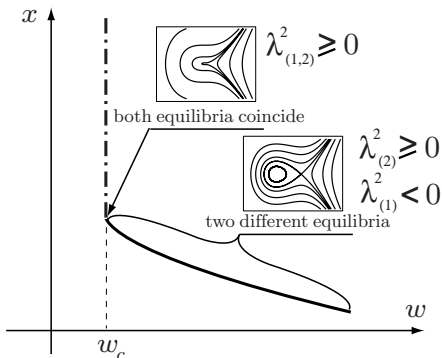
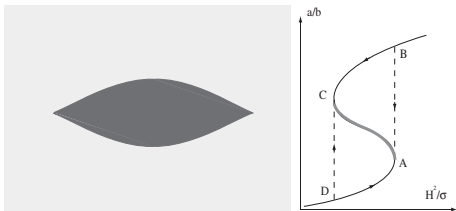


Figure: Critical curve in the (x, w) -plane: on the dynamic bifurcation; solid black line represents stable equilibria, dot-dash line is a dynamic bifurcation when bubble grows indefinitely with time. λ 's are the eigenvalues of the linearization around equilibrium points.

Hysteresis

Motivation from real bubbles

● Ferrofluid drop in a magnetic field^a

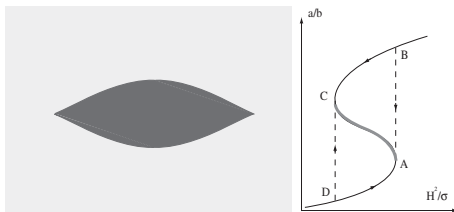


^aBacri & Salin, 1982

Hysteresis

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● Ferrofluid drop in a magnetic field^a



- Total energy $E_t = E_s + E_m$ is a sum of magnetic E_m and interfacial E_s contributions:

$$E_s = \sigma 2\pi a^2 e [e + \epsilon^{-1} \sin^{-1} \epsilon], \quad \epsilon = \sqrt{1 - e^2}$$

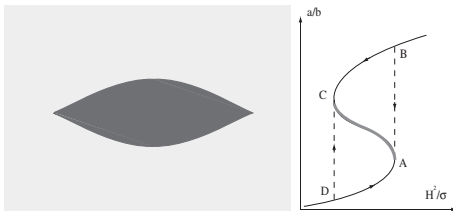
$$E_m = -\frac{VH^2}{8\pi} \frac{\mu_1}{\alpha + n}, \quad \alpha = \frac{\mu_1}{\mu_2 - \mu_1}.$$

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Hysteresis

Motivation from real bubbles

● Ferrofluid drop in a magnetic field^a



- Total energy $E_t = E_s + E_m$ is a sum of magnetic E_m and interfacial E_s contributions:

$$E_s = \sigma 2\pi a^2 e [e + \epsilon^{-1} \sin^{-1} \epsilon], \quad \epsilon = \sqrt{1 - e^2}$$

$$E_m = -\frac{VH^2}{8\pi} \frac{\mu_1}{\alpha + n}, \quad \alpha = \frac{\mu_1}{\mu_2 - \mu_1}.$$

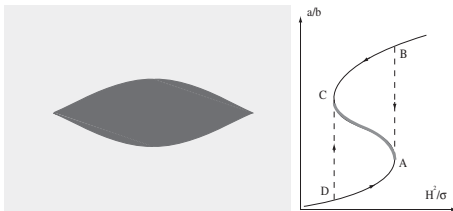
- Minimizing E_t produces $H^2/\sigma = g(e)$.

^aBacri & Salin, 1982

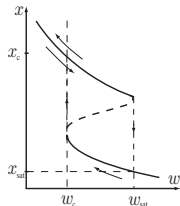
Hysteresis

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● Conjecture



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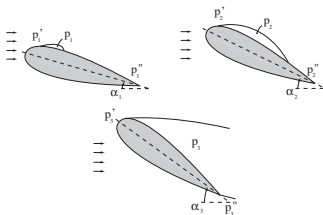
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Hysteresis

Motivation: separation vs. cavitating bubble

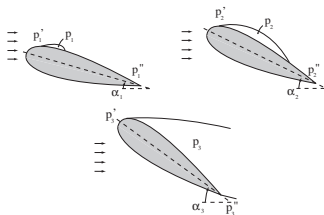
● Separation bubble:



Hysteresis

Motivation: separation vs. cavitating bubble

● Separation bubble:



● On mechanism of separation

$$p_1' - p_1'' < p_2' - p_2'' < p_3' - p_3'',$$

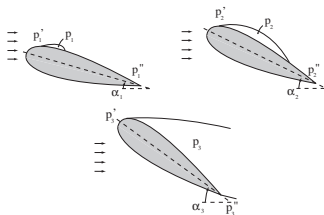
$$l_1 < l_2 < l_3.$$

$p_1 > p_2 > p_3$ with $p_i < p_i'$, $i = 1, 2, 3$.

Hysteresis

Motivation: separation vs. cavitating bubble

● Separation bubble:



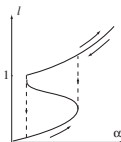
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$$p_1 > p_2 > p_3 \text{ with } p_i < p_i', \quad i = 1, 2, 3.$$

● Cavitating bubble:

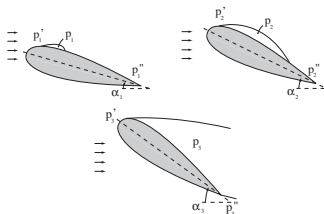


Acosta (1955), Tulin (1953)

Hysteresis

Motivation: separation vs. cavitating bubble

● Separation bubble:



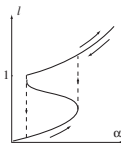
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$$p_1 > p_2 > p_3 \text{ with } p_i < p_i', \quad i = 1, 2, 3.$$

● Cavitating bubble:



Acosta (1955), Tulin (1953)

- The behavior of a cavitation bubble is given by for partially cavitating, $l < 1$, and supercavitating, $l > 1$, foils respectively,

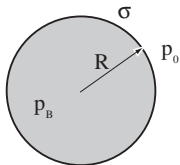
$$\frac{\chi}{2\alpha} = \frac{2 - l + 2(1 - l)^{1/2}}{l^{1/2}(1 - l)^{1/2}}, \quad l < 1,$$

$$\alpha \left(\frac{2}{\chi} + 1 \right) = (1 - l)^{1/2}, \quad l > 1,$$

Hysteresis

Motivation: static vs. cavitating bubble

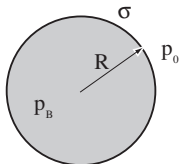
- **Static bubble:**



Hysteresis

Motivation: static vs. cavitating bubble

- **Static bubble:**



- Real static bubble behavior

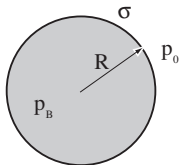
$$p_B = 2\sigma/R + p_0,$$

where p_B is the pressure inside the bubble, p_0 – pressure outside the bubble, $\sigma > 0$ is the interfacial tension, and R is a radius of the bubble.

Hysteresis

Motivation: static vs. cavitating bubble

- **Static bubble:**

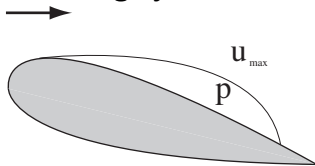


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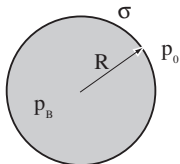
- **Cavitating hydrofoil:**



Hysteresis

Motivation: static vs. cavitating bubble

- **Static bubble:**

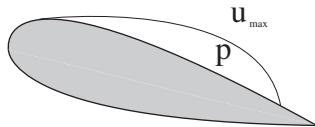


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$$p_B = 2\sigma/R + p_0,$$

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- **Cavitating hydrofoil:**



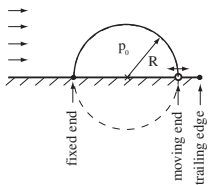
- Bubble behavior:

$$p + \rho u^2/2 = p_{st},$$

where p is a dynamic pressure, and p_{st} is the pressure of a fluid at rest (at stagnation point).

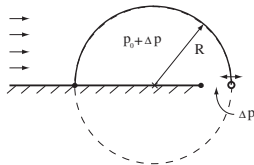
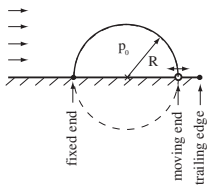
Hysteresis

Mechanical model of hysteresis: elastic bubble



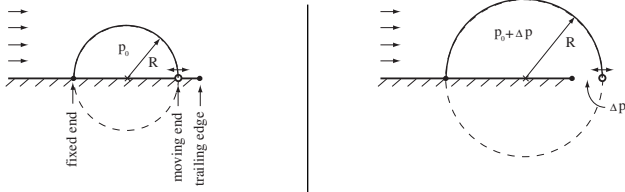
Hysteresis

Mechanical model of hysteresis: elastic bubble



Hysteresis

Mechanical model of hysteresis: elastic bubble



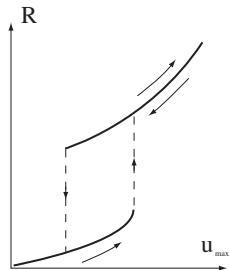
The mechanical analog of a bubble:

$$p = p_0 + \tilde{\sigma}/R, \quad p > p_0,$$

i.e. the bubble grows when the ambient pressure, $p = p_{st} - \rho u_{max}^2/2$, decreases.

$$u_{max}^{cr, >} : R_0 = \tilde{\sigma} \left[p_{st} - p_0 - \rho |u_{max}^{cr, >}|^2/2 \right]^{-1}$$

$$u_{max}^{cr, <} : R_0 = \tilde{\sigma} \left[p_{st} - p_0 - \Delta p_0 - \rho |u_{max}^{cr, <}|^2/2 \right]^{-1}$$



Hysteresis

Model: potential function $V(x)$ approach

Modified model:

$$\ddot{x} + \mu \dot{x} = -V_x(x; \alpha, w).$$

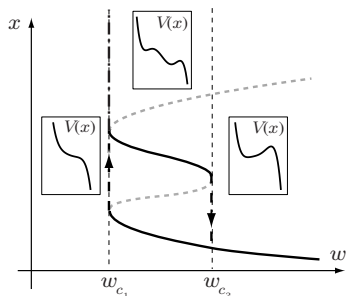


Figure: Hysteresis curve in the (x, w) -plane and corresponding potential functions; solid black lines represent stable equilibria, while dashed lines are unstable equilibria; dot-dash line represents a dynamic bifurcation (bubble size grows with time unboundedly).

Conclusions

- A new physically motivated low-dimensional model of separation bubble dynamics was constructed by contrasting and appealing to similarities with actual bubble dynamics^a. The latter suggested
 - the proper choice of coarse variables and primary bifurcation;
 - an explanation of the nature of the hysteresis.
- Suggestions for experimental studies to improve the model:
 - investigate the finite amplitude stability of separation bubbles;
 - determine the form of the state equation for separation bubble.
- Open issues:
 - rigorous derivation of the low-dim model by *coarsening* NSEs;
 - more close connection with experimental observations and development of a *calibration procedure*.

Acknowledgements. R.K. would like to thank Prof. Anatol Roshko for stimulating discussions.

^aKrechetnikov, Marsden, Nagib, *Physica D* 238, 1152 (2009)